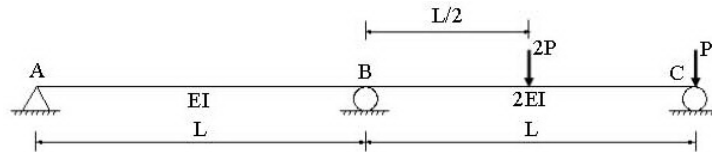
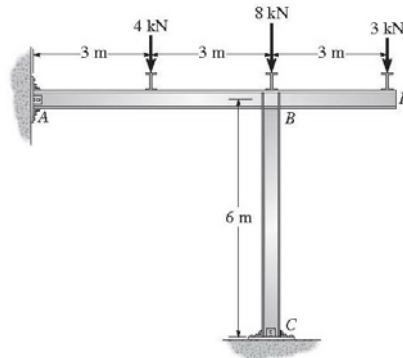


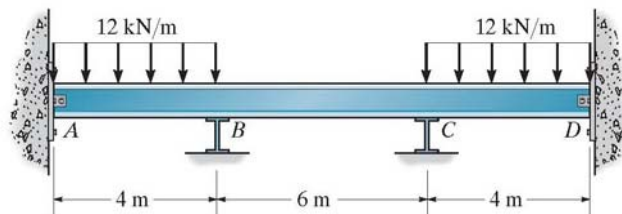
1. 請以傾角變位法(slope-deflection method)分析下圖梁結構，試求 A、B 及 C 點之反力並繪製剪力圖與彎矩圖，假設所有桿件之 $EI = \text{constant}$ 。(20 分)



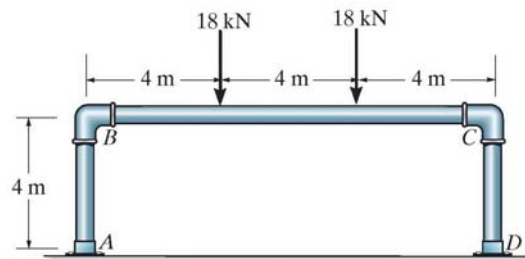
2. 如下圖，假設支承 A 與 C 點及接點 B 為固定連接，且 EI 為定值，試以傾角變位法(slope-deflection method)求出剛架各構件末端的彎矩。(20 分)



3. 如下圖，若 EI 為定值，假設 B 與 C 點為滾支承，A 與 D 點為樞支承，試以彎矩分配法求出 B 及 C 處的彎矩，並繪出該梁的彎矩圖。(20 分)

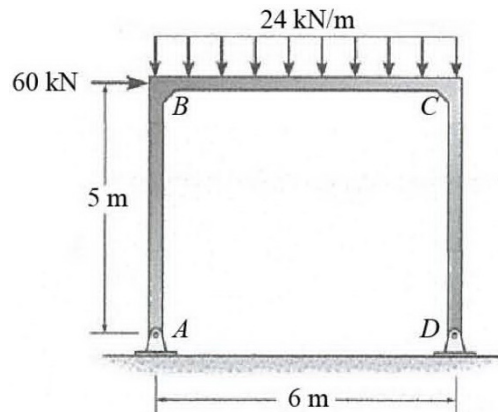


4. 如下圖，剛架由固定連接的管子製成，設 EI 為定值，若承受如圖所示之載重，試以彎矩分配法求出在各接點和支承處產生的彎矩。(20 分)



5. 如下圖，若 EI 為定值

- (1) 限以傾角變位法求各端點彎矩與構架的側位移。(16 分)
- (2) 限以彎矩分配法求各端點彎矩與構架的側位移。(16 分)。
- (3) 請畫出此構架的剪力圖與彎矩圖。(8 分)



6. 請問上完這學期結構學後有何心得與建議? (10%)

參考公式:

固端彎矩

$$(FEM)_{AB} = \frac{PL}{8} \quad (FEM)_{BA} = \frac{PL}{8}$$

$$(FEM)'_{AB} = \frac{3PL}{16}$$

$$(FEM)_{AB} = \frac{Pb^2a}{L^2} \quad (FEM)_{BA} = \frac{Pa^2b}{L^2}$$

$$(FEM)'_{AB} = \left(\frac{P}{L^2}\right)\left(b^2a + \frac{a^2b}{2}\right)$$

$$(FEM)_{AB} = \frac{wL^2}{12} \quad (FEM)_{BA} = \frac{wL^2}{12}$$

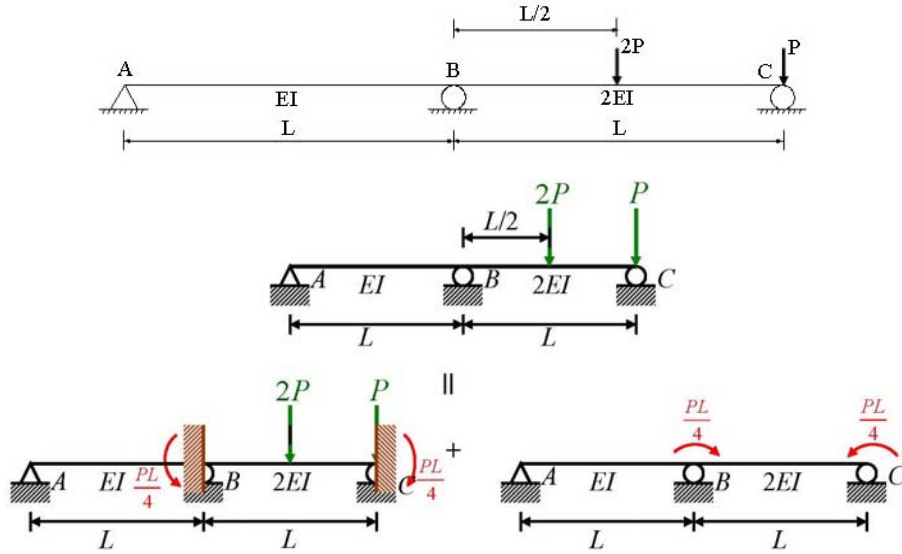
$$(FEM)'_{AB} = \frac{wL^2}{8}$$

$$(FEM)_{AB} = \frac{6EI\Delta}{L^2} \quad (FEM)_{BA} = \frac{6EI\Delta}{L^2}$$

$$(FEM)'_{AB} = \frac{3EI\Delta}{L^2}$$

參考解答:

1. 請以傾角變位法(slope-deflection method)分析下圖梁結構，試求 A、B 及 C 點之反力。假設梁之 $EI = \text{constant}$ 。(20 分)

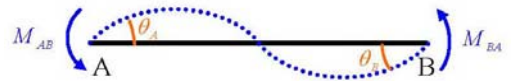


$$(FEM)_{BC} = \frac{PL}{4}, (FEM)_{CB} = -\frac{PL}{4} \quad (\text{正表示逆時鐘方向，負表示順時鐘方向})$$

AB 段 ($M_{AB} = 0$)

$$M_{AB} = \frac{4EI}{L}\theta_A + \frac{2EI}{L}\theta_B \Rightarrow \theta_A = -\frac{1}{2}\theta_B$$

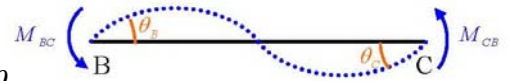
$$M_{BA} = \frac{2EI}{L}\theta_A + \frac{4EI}{L}\theta_B = \frac{3EI}{L}\theta_B$$



BC 段 ($M_{CB} = \frac{PL}{4}$)

$$M_{BC} = \frac{4(2EI)}{L}\theta_B + \frac{2(2EI)}{L}\theta_C = \frac{8EI}{L}\theta_B + \frac{4EI}{L}\theta_C$$

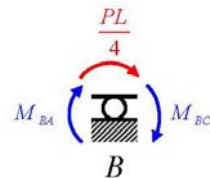
$$M_{CB} = \frac{2(2EI)}{L}\theta_B + \frac{4(2EI)}{L}\theta_C \Rightarrow \theta_C = \frac{PL^2}{32EI} - \frac{1}{2}\theta_B$$



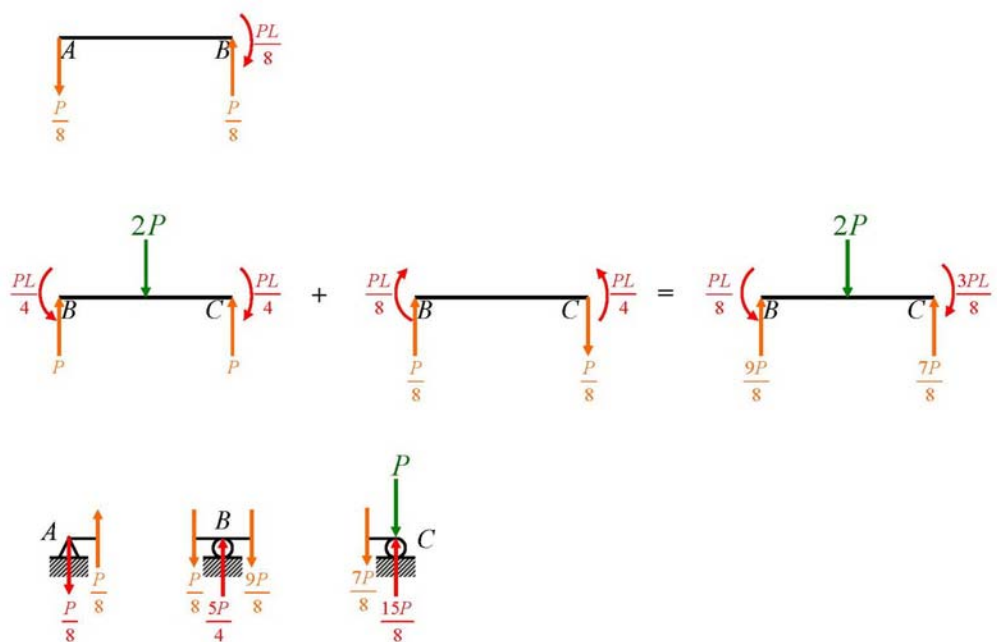
$$\text{代回 } M_{BC} \text{ 可得 } M_{BC} = \frac{6EI}{L}\theta_B + \frac{PL}{8}$$

$$\text{取 } B \text{ 節點彎矩平衡: } M_{BA} + M_{BC} + \frac{PL}{4} = 0 \Rightarrow \theta_B = -\frac{PL^2}{24EI}$$

$$\therefore \theta_A = -\frac{1}{2}\theta_B = \frac{PL^2}{48EI}, \quad \theta_C = \frac{PL^2}{32EI} - \frac{1}{2}\theta_B = \frac{5PL^2}{96EI}$$



$$\text{故可得 } M_{BA} = \frac{3EI}{L}\theta_B = -\frac{PL}{8}, \quad M_{BC} = \frac{6EI}{L}\theta_B + \frac{PL}{8} = -\frac{PL}{8}$$

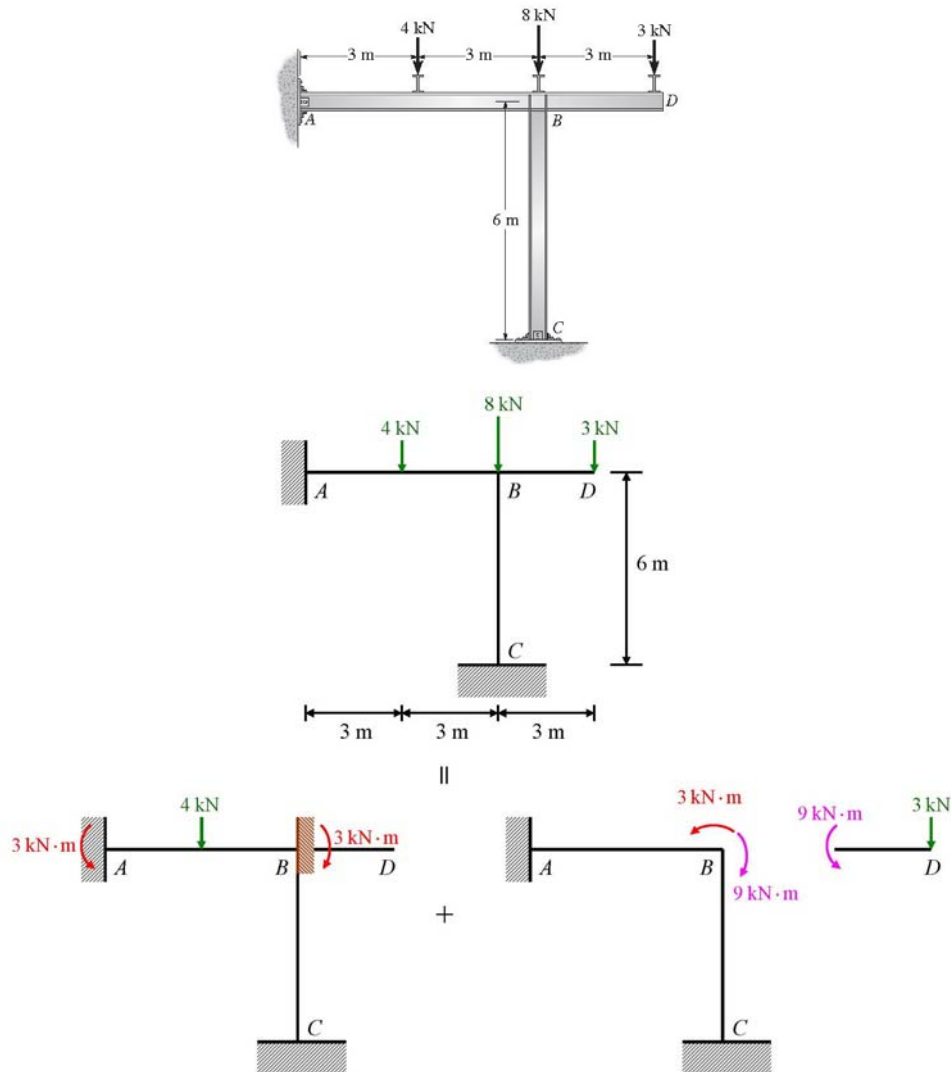


A 點反力 $\frac{P}{8}$ (向下)

B 點反力 $\frac{5P}{4}$ (向上)

C 點反力 $\frac{15P}{8}$ (向上)

2. 如下圖，假設支承 A 與 C 點及接點 B 為固定連接，且 EI 為定值，試以傾角變位法(slope-deflection method)求出剛架各構件末端的彎矩。(20 分)



由圖可知 A 與 C 端皆為固定端，即 $\theta_A = 0$ 與 $\theta_C = 0$

AB 段 ($\theta_A = 0$)

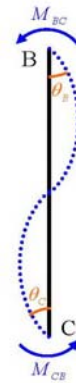
$$M_{AB} = \frac{4EI}{L}\theta_A + \frac{2EI}{L}\theta_B \Rightarrow M_{AB} = \frac{EI}{3}\theta_B$$

$$M_{BA} = \frac{2EI}{L}\theta_A + \frac{4EI}{L}\theta_B = \frac{3EI}{L}\theta_B \Rightarrow M_{BA} = \frac{2EI}{3}\theta_B$$

BC 段 ($\theta_C = 0$)

$$M_{BC} = \frac{4EI}{L}\theta_B + \frac{2EI}{L}\theta_C \Rightarrow M_{BC} = \frac{2EI}{3}\theta_B$$

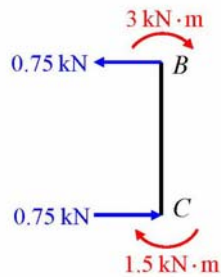
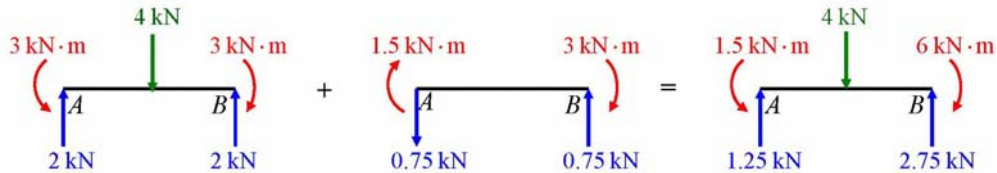
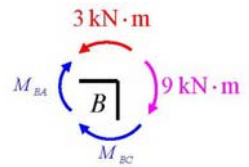
$$M_{CB} = \frac{2EI}{L}\theta_B + \frac{4EI}{L}\theta_C \Rightarrow M_{CB} = \frac{EI}{3}\theta_B$$



取 B 節點彎矩平衡: $M_{BA} + M_{BC} - 3 + 9 = 0 \Rightarrow \theta_B = -\frac{9}{2EI}$

$\therefore M_{AB} = \frac{EI}{3}\theta_B = -1.5 \text{ (kN} \cdot \text{m)}, \quad M_{BA} = \frac{2EI}{3}\theta_B = -3 \text{ (kN} \cdot \text{m)}$

$M_{BC} = \frac{2EI}{3}\theta_B = -3 \text{ (kN} \cdot \text{m)}, \quad M_{CB} = \frac{EI}{3}\theta_B = -1.5 \text{ (kN} \cdot \text{m)}$



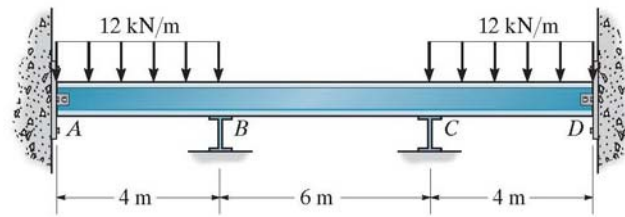
$\therefore M_{AB} = 1.5 \text{ (kN} \cdot \text{m) (逆時鐘方向)}$

$M_{BA} = 6 \text{ (kN} \cdot \text{m) (順時鐘方向)}$

$M_{BC} = 3 \text{ (kN} \cdot \text{m) (順時鐘方向)}$

$M_{CB} = 1.5 \text{ (kN} \cdot \text{m) (順時鐘方向)}$

3. 如下圖，若 EI 為定值，假設 B 與 C 點為滾支承， A 與 D 點為樞支承，試以彎矩分配法求出 B 及 C 處的彎矩，並繪出該梁的彎矩圖。(20 分)



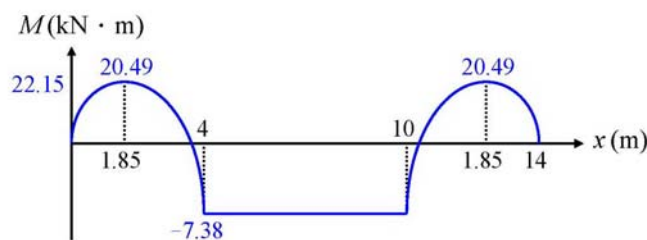
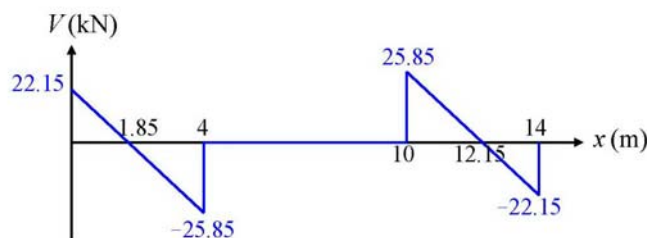
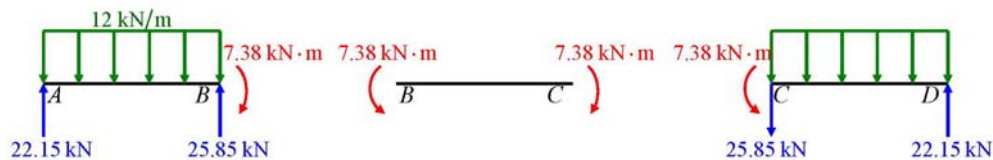
由圖可知此為對稱結構

$$(FEM)_{BA} = -\frac{w\ell^2}{8} = -\frac{12 \cdot 4^2}{8} = -24 \text{ (kN} \cdot \text{m)},$$

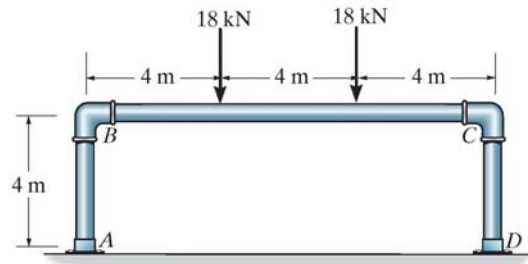
$$k_{BA} = \frac{3}{4} \cdot \frac{4EI}{\ell_{AB}} = \frac{3}{4}EI, \quad k_{BC} = \frac{1}{2} \cdot \frac{4EI}{\ell_{BC}} = \frac{EI}{3}$$

$$DF_{BA} = \frac{\frac{3}{4}}{\frac{3}{4} + \frac{1}{3}} = \frac{9}{13} = 0.6923, \quad DF_{BC} = \frac{\frac{1}{3}}{\frac{3}{4} + \frac{1}{3}} = \frac{4}{13} = 0.3077$$

節點	A	B	
構件	AB	BA	BC
DF	1	$\frac{9}{13}$	$\frac{4}{13}$
FEM		-24	
D1		16.62	7.38
$\sum M$		-7.38	7.38



4. 如下圖，剛架由固定連接的管子製成，設 EI 為定值，若承受如圖所示之載重，試以彎矩分配法求出在各接點和支承處產生的彎矩。(20 分)



由圖可知此為對稱結構

$$(FEM)_{BC} = \frac{18 \cdot 4 \cdot 8^2}{12} + \frac{18 \cdot 4^2 \cdot 8}{12} = 48 \text{ (kN} \cdot \text{m)},$$

$$(FEM)_{CB} = -48 \text{ (kN} \cdot \text{m)}$$

$$k_{BA} = \frac{4EI}{\ell_{AB}} = EI, \quad k_{BC} = \frac{1}{2} \cdot \frac{4EI}{\ell_{BC}} = \frac{EI}{6}$$

$$DF_{BA} = \frac{1}{1 + \frac{1}{6}} = \frac{6}{7} = 0.8571, \quad DF_{BC} = \frac{\frac{1}{6}}{1 + \frac{1}{6}} = \frac{1}{7} = 0.1429$$

節點	A	B	
構件	AB	BA	BC
DF	0	$\frac{6}{7}$	$\frac{1}{7}$
FEM			48
D1		-41.14	-6.86
C1	-20.57		
$\sum M$	-20.57	-41.14	41.14

$$\therefore M_{AB} = 20.57 \text{ (kN} \cdot \text{m)} \text{ (順時鐘方向)}$$

$$M_{BA} = 41.14 \text{ (kN} \cdot \text{m)} \text{ (順時鐘方向)}$$

$$M_{BC} = 41.14 \text{ (kN} \cdot \text{m)} \text{ (逆時鐘方向)}$$

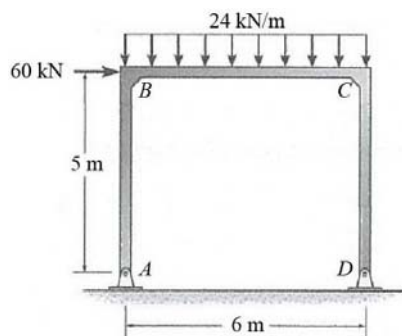
$$M_{CB} = 41.14 \text{ (kN} \cdot \text{m)} \text{ (順時鐘方向)}$$

$$M_{CD} = 41.14 \text{ (kN} \cdot \text{m)} \text{ (逆時鐘方向)}$$

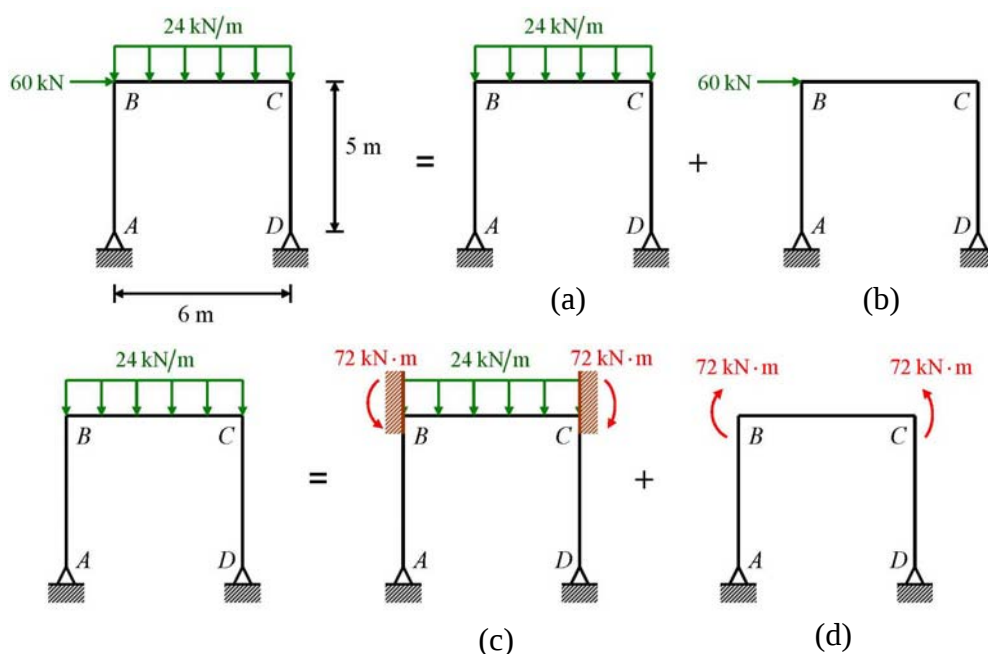
$$M_{DC} = 20.57 \text{ (kN} \cdot \text{m)} \text{ (逆時鐘方向)}$$

5. 如下圖，若 EI 為定值

- (1) 限以傾角變位法求各端點彎矩與構架的側位移。(16 分)
- (2) 限以彎矩分配法求各端點彎矩與構架的側位移。(16 分)。
- (3) 請畫出此構架的剪力圖與彎矩圖。(8 分)



(1)



$$(FEM)_{BC} = \frac{w\ell^2}{12} = \frac{24 \cdot 6^2}{12} = 72 \text{ (kN} \cdot \text{m)}, \quad (FEM)_{CB} = -72 \text{ (kN} \cdot \text{m)}$$

先計算圖(d)，由圖可知 A 與 D 端皆為樞接，即 $M_{AB} = 0$ 與 $M_{DC} = 0$

AB 段 ($M_{AB} = 0$)

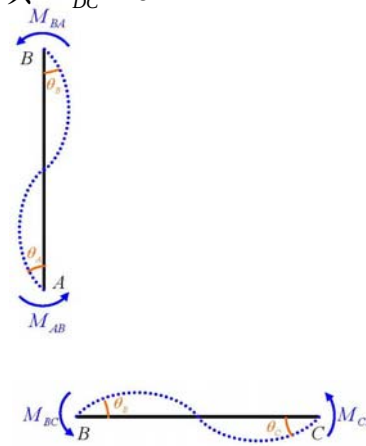
$$M_{AB} = \frac{4EI}{L}\theta_A + \frac{2EI}{L}\theta_B \Rightarrow \theta_A = -\frac{1}{2}\theta_B$$

$$M_{BA} = \frac{2EI}{L}\theta_A + \frac{4EI}{L}\theta_B \Rightarrow M_{BA} = \frac{3EI}{5}\theta_B$$

BC 段

$$M_{BC} = \frac{4EI}{L}\theta_B + \frac{2EI}{L}\theta_C \Rightarrow M_{BC} = \frac{2EI}{3}\theta_B + \frac{EI}{3}\theta_C$$

$$M_{CB} = \frac{2EI}{L}\theta_B + \frac{4EI}{L}\theta_C \Rightarrow M_{CB} = \frac{EI}{3}\theta_B + \frac{2EI}{3}\theta_C$$

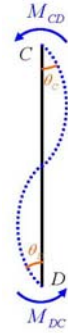


CD 段 ($M_{DC} = 0$)

$$M_{CD} = \frac{4EI}{L}\theta_C + \frac{2EI}{L}\theta_D \Rightarrow M_{CD} = \frac{4EI}{5}\theta_C + \frac{2EI}{5}\theta_D$$

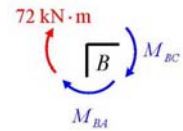
$$M_{DC} = \frac{2EI}{L}\theta_C + \frac{4EI}{L}\theta_D \Rightarrow \theta_D = -\frac{1}{2}\theta_C$$

$$\text{代回 } M_{CD} \text{ 可得 } M_{CD} = \frac{3EI}{5}\theta_C$$



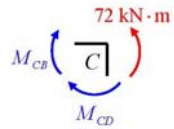
取 B 節點彎矩平衡:

$$M_{BA} + M_{BC} + 72 = 0 \Rightarrow \frac{19EI}{15}\theta_B + \frac{EI}{3}\theta_C = -72 \quad \dots (1)$$



取 C 節點彎矩平衡:

$$M_{CB} + M_{CD} - 72 = 0 \Rightarrow \frac{EI}{3}\theta_B + \frac{19EI}{15}\theta_C = 72 \quad \dots (2)$$

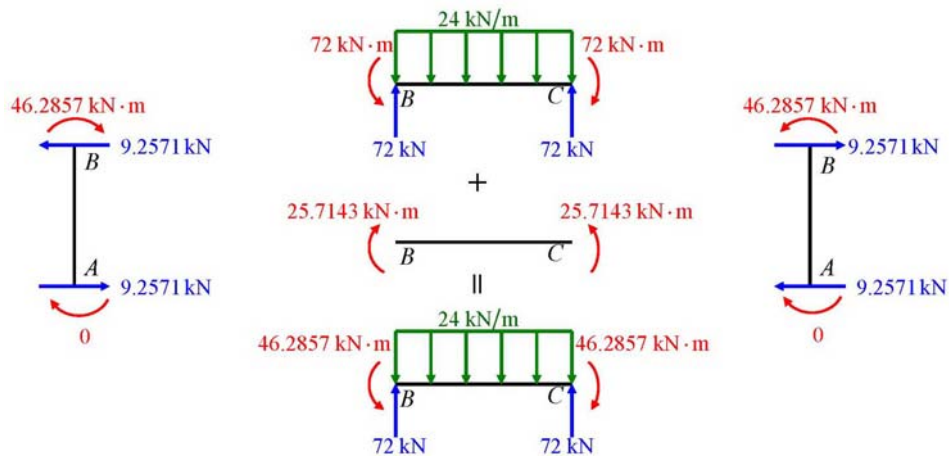


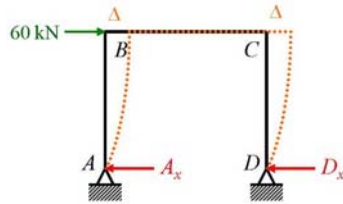
由(1)、(2)可得 $\theta_C = -\theta_B = \frac{540}{7EI}$, $\theta_D = -\frac{1}{2}\theta_C = -\frac{270}{7EI}$

$$\therefore M_{AB} = 0, \quad M_{BA} = -\frac{324}{7} = -46.2857 \text{ (kN} \cdot \text{m)},$$

$$M_{BC} = -\frac{180}{7} = -25.7143 \text{ (kN} \cdot \text{m)}, \quad M_{CB} = \frac{180}{7} = 25.7143 \text{ (kN} \cdot \text{m)}$$

$$M_{CD} = \frac{324}{7} = 46.2857 \text{ (kN} \cdot \text{m)}, \quad M_{DC} = 0$$





再計算圖(b)，由圖可知 A 與 D 端皆為樞接，即 $M_{AB} = 0$ 與 $M_{DC} = 0$ ，
且 AB、CD 段有側向位移 Δ ，BC 段無側向位移。

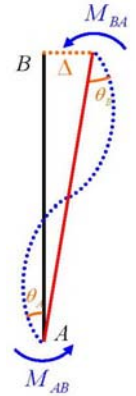
AB 段 ($M_{AB} = 0$)

$$M_{AB} = \frac{4EI}{L}\theta_A + \frac{2EI}{L}\theta_B + \frac{6EI}{L}\left(\frac{\Delta}{L}\right) \Rightarrow 0 = \frac{4EI}{5}\theta_A + \frac{2EI}{5}\theta_B + \frac{6EI}{25}\Delta$$

$$\Rightarrow \theta_A = -\left(\frac{1}{2}\theta_B + \frac{3}{10}\Delta\right)$$

$$M_{BA} = \frac{2EI}{L}\theta_A + \frac{4EI}{L}\theta_B + \frac{6EI}{L}\left(\frac{\Delta}{L}\right) \Rightarrow M_{BA} = \frac{2EI}{5}\theta_A + \frac{4EI}{5}\theta_B + \frac{6EI}{25}\Delta$$

$$\Rightarrow M_{BA} = \frac{3EI}{5}\theta_B + \frac{3EI}{25}\Delta$$



BC 段

$$M_{BC} = \frac{4EI}{L}\theta_B + \frac{2EI}{L}\theta_C \Rightarrow M_{BC} = \frac{2EI}{3}\theta_B + \frac{EI}{3}\theta_C$$

$$M_{CB} = \frac{2EI}{L}\theta_B + \frac{4EI}{L}\theta_C \Rightarrow M_{CB} = \frac{EI}{3}\theta_B + \frac{2EI}{3}\theta_C$$



CD 段 ($M_{DC} = 0$)

$$M_{CD} = \frac{4EI}{L}\theta_C + \frac{2EI}{L}\theta_D + \frac{6EI}{L}\left(\frac{\Delta}{L}\right) \Rightarrow M_{CD} = \frac{4EI}{5}\theta_C + \frac{2EI}{5}\theta_D + \frac{6EI}{25}\Delta$$

$$M_{DC} = \frac{2EI}{L}\theta_C + \frac{4EI}{L}\theta_D + \frac{6EI}{L}\left(\frac{\Delta}{L}\right) \Rightarrow \frac{2EI}{5}\theta_C + \frac{4EI}{5}\theta_D + \frac{6EI}{25}\Delta = 0$$

$$\Rightarrow \theta_D = -\left(\frac{1}{2}\theta_C + \frac{3}{10}\Delta\right)$$

$$\text{代回 } M_{CD} \text{ 可得 } M_{CD} = \frac{3EI}{5}\theta_C + \frac{3EI}{25}\Delta$$

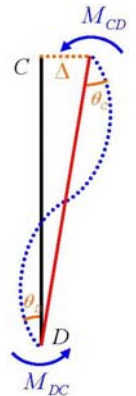
取 B 節點彎矩平衡:

$$M_{BA} + M_{BC} = 0 \Rightarrow \frac{19EI}{15}\theta_B + \frac{EI}{3}\theta_C + \frac{3EI}{25}\Delta = 0 \quad \dots (1)$$

取 C 節點彎矩平衡:

$$M_{CB} + M_{CD} = 0 \Rightarrow \frac{EI}{3}\theta_B + \frac{19EI}{15}\theta_C + \frac{3EI}{25}\Delta = 0 \quad \dots (2)$$

$$\text{由力平衡: } \sum F_x = 0 \Rightarrow A_x + D_x = 60$$



$$\text{又 } A_x = \frac{M_{BA}}{L} = \frac{3EI}{25}\theta_B + \frac{3EI}{125}\Delta$$

$$D_x = \frac{M_{CD}}{L} = \frac{3EI}{25}\theta_C + \frac{3EI}{125}\Delta$$

$$\therefore A_x + D_x = 60 \Rightarrow \frac{3EI}{25}\theta_B + \frac{3EI}{25}\theta_C + \frac{6EI}{125}\Delta = 60 \quad \dots (3)$$

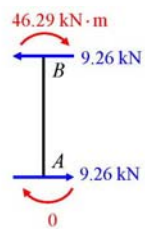
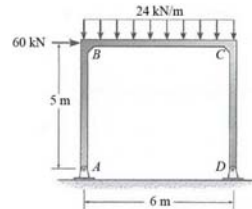
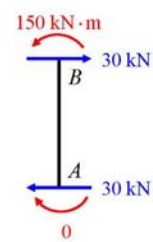
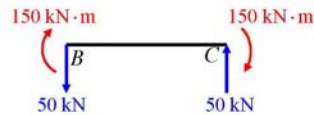
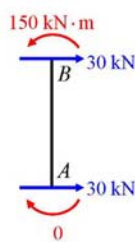
$$\text{由(1)(2)(3)可得 } \theta_C = \theta_B = -\frac{150}{EI}, \Delta = -\frac{40}{3}\theta_C = \frac{2000}{EI}$$

$$\therefore M_{BA} = \frac{3EI}{5}\theta_B + \frac{3EI}{25}\Delta = 150 \text{ (kN} \cdot \text{m)}$$

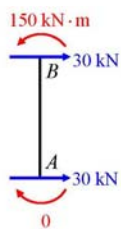
$$M_{BC} = \frac{2EI}{3}\theta_B + \frac{EI}{3}\theta_C = -150 \text{ (kN} \cdot \text{m)}$$

$$M_{CB} = \frac{EI}{3}\theta_B + \frac{2EI}{3}\theta_C = -150 \text{ (kN} \cdot \text{m)}$$

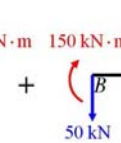
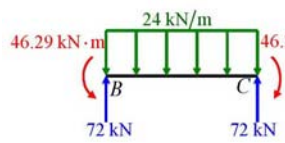
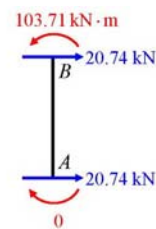
$$M_{CD} = \frac{3EI}{5}\theta_C + \frac{3EI}{25}\Delta = 150 \text{ (kN} \cdot \text{m)}$$



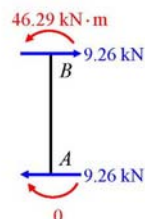
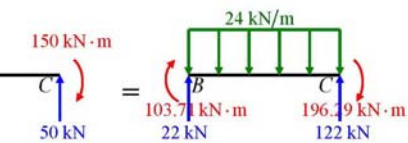
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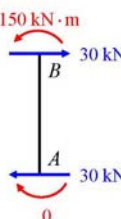
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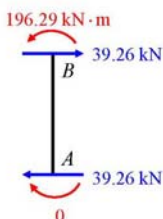
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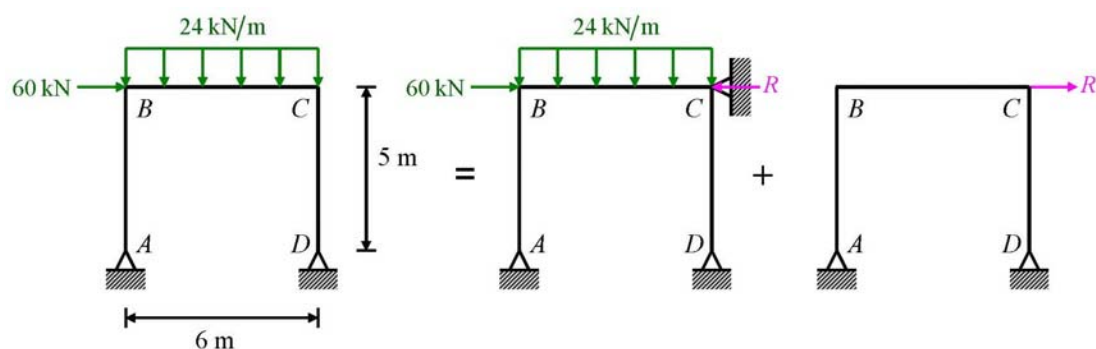
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(2)



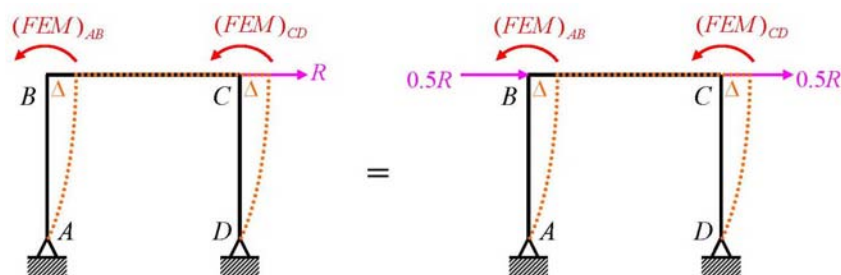
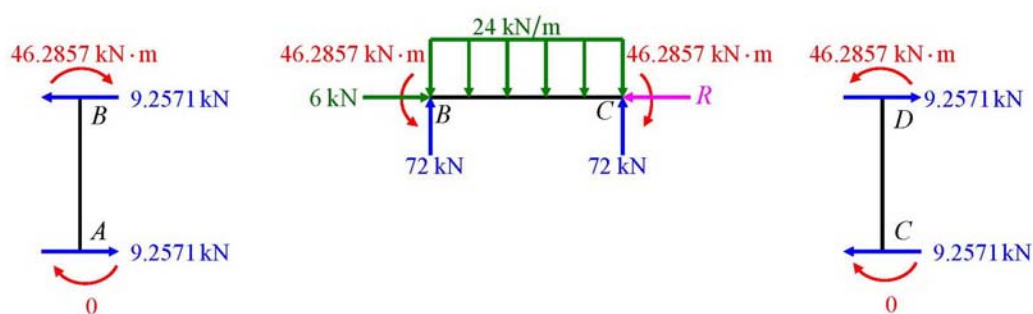
上圖無側向位移唯一可能為對稱，即反力 $R = 60$ (kN)

$$(FEM)_{BC} = \frac{w\ell^2}{12} = \frac{24 \cdot 6^2}{12} = 72 \text{ (kN} \cdot \text{m)}, \quad (FEM)_{CB} = -72 \text{ (kN} \cdot \text{m)}$$

$$k_{BA} = \frac{3}{4} \cdot \frac{4EI}{L_{AB}} = \frac{3EI}{5}, \quad k_{BC} = \frac{1}{2} \cdot \frac{4EI}{L_{BC}} = \frac{EI}{3}$$

$$DF_{BA} = \frac{k_{BA}}{k_{BA} + k_{BC}} = \frac{9}{14} = 0.6429, \quad DF_{BC} = \frac{k_{BC}}{k_{BA} + k_{BC}} = \frac{5}{14} = 0.3571$$

節點	A	B	
構件	AB	BA	BC
DF	1	0.6429	0.3571
FEM			72
D1		-46.2857	-25.7143
$\sum M$		-46.2857	46.2857



由圖可知此為反對稱

$$(\text{FEM})_{BA} = (\text{FEM})_{CD} = \frac{3EI\Delta}{L^2}$$

$$k_{BA} = \frac{3}{4} \cdot \frac{4EI}{L_{AB}} = \frac{3EI}{5}, \quad k_{BC} = \frac{3}{2} \cdot \frac{4EI}{L_{BC}} = EI$$

$$DF_{BA} = \frac{k_{BA}}{k_{BA} + k_{BC}} = \frac{3}{8} = 0.375, \quad DF_{BC} = \frac{k_{BC}}{k_{BA} + k_{BC}} = \frac{5}{8} = 0.625$$

節點	A	B	
構件	AB	BA	BC
DF	1	0.375	0.625
FEM		3	
D1		-1.125	-1.875
$\sum M$		1.875	-1.875

$$\sum F_x = 0 \Rightarrow 0.375 \frac{EI\Delta}{L^2} + 0.375 \frac{EI\Delta}{L^2} - R = 0 \Rightarrow \Delta = \frac{4}{3} \cdot \frac{RL^2}{EI} = \frac{2000}{EI}$$

$$M_{BA} = 1.875 \frac{EI\Delta}{L^2} = 150 \text{ (kN} \cdot \text{m)}$$

$$M_{BC} = -1.875 \frac{EI\Delta}{L^2} = -150 \text{ (kN} \cdot \text{m)}$$

$$M_{CB} = -1.875 \frac{EI\Delta}{L^2} = -150 \text{ (kN} \cdot \text{m)}$$

$$M_{CD} = 1.875 \frac{EI\Delta}{L^2} = 150 \text{ (kN} \cdot \text{m)}$$

