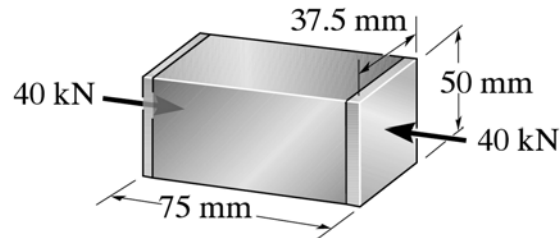
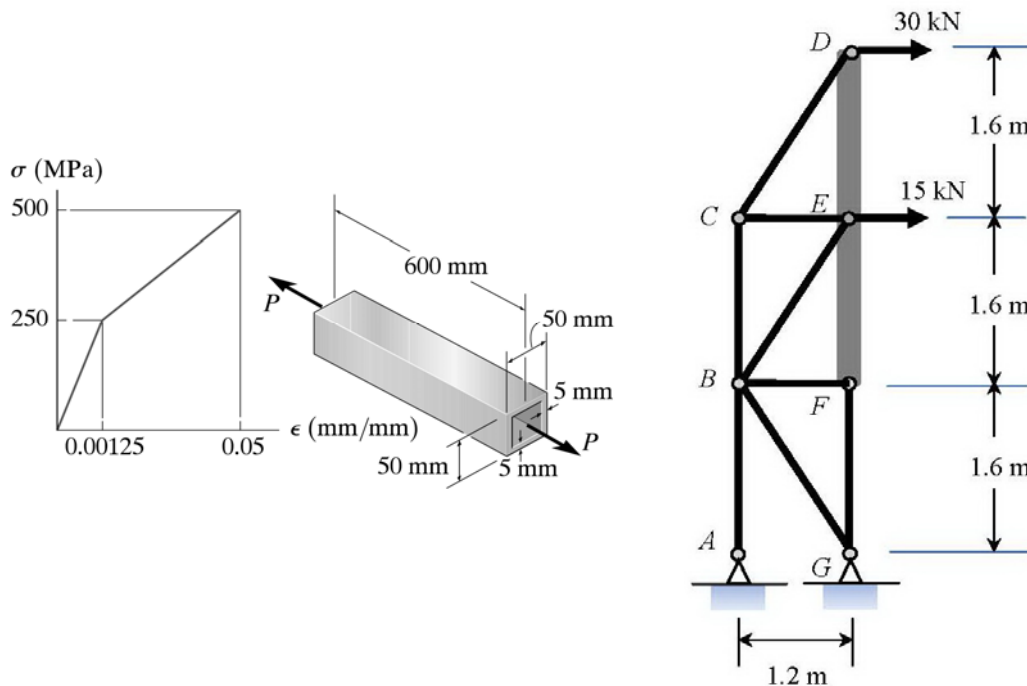


1. 鋁塊有矩形截面，受一軸向壓縮力 40 kN 作用。若 37.5 mm 的邊長度為 37.5033 mm，試求泊松比及 50 mm 邊的新長度。 $E_{al} = 70 \text{ GPa}$ 。(20%)



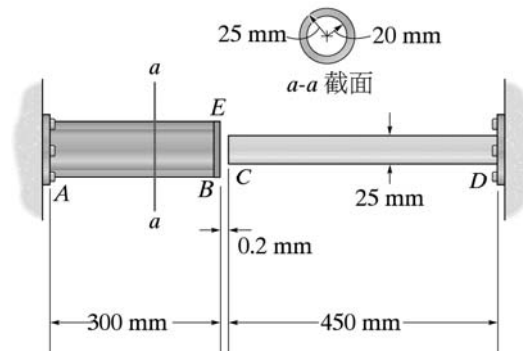
2. (1) 當一軸向負載 $P = 100 \text{ kN}$ 施加在一方形中空棒，試求其伸長量。(7%)
 (2) 若此負載增加至 $P = 360 \text{ kN}$ 然後釋放，試求其永久伸長量。(8%)
 (棒材之應力 - 應變近似圖如下左圖。)



3. DEF 為一剛性桿件 (rigid bar) 且由一桁架系統支撐 (如上右圖)。若桁架中各桿件之剪彈性模數 (shear modulus) $G = 77.2 \text{ GPa}$ ，泊松比 (Poisson's ratio) $\nu = 0.3$ ，且容許正向應力 (allowable normal stress) 為 120 MPa。
 (1) 請求出點 A 及 G 之反力。(5%)
 (2) 請問在考慮容許正向應力條件下， BG 桿之最小斷面積。(10%)
 (3) 若 FG 為直徑 40 mm 之實心桿件，請問 FG 桿之變形量？(10%)

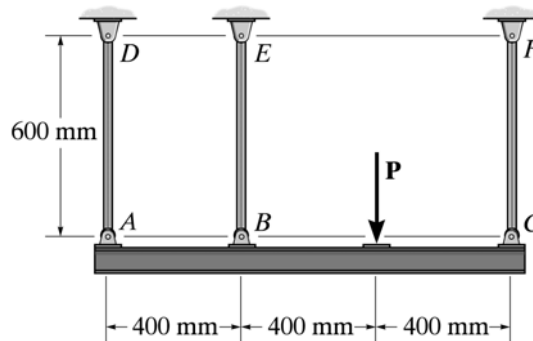
4. AM1004-T61 鎂合金管 AB 與剛性板 E 固定在一起， E 端和 6016-T6 鋁合金實心圓桿 CD 的 C 端間的間隙為 0.2 mm ，其溫度為 30°C 。若溫度上升至 80°C 時，剛性端蓋厚可忽略

- (1) 試求管與桿件中的正應力。(10%)
 - (2) 若管或桿件不發生降伏的情形下，溫度最高可上升至多少 $^\circ\text{C}$ 。(10%)
- (鎂: $\alpha_{ma} = 26 \cdot 10^{-6} / ^\circ\text{C}$, $E_{ma} = 44.7\text{ GPa}$, $(\sigma_Y)_{ma} = 152\text{ MPa}$)
 (鋁: $\alpha_{al} = 24 \cdot 10^{-6} / ^\circ\text{C}$, $E_{al} = 68.9\text{ GPa}$, $(\sigma_Y)_{al} = 255\text{ MPa}$)



5. 剛性樑由三根直徑 25 mm 的 A-36 鋼桿支撐。若樑支承一 $P = 230\text{ kN}$ 的負載，

- (1) 試求每一鋼桿所受的力。(10%)
 - (2) 若負載 $P = 230\text{ kN}$ 釋放時，試求每一鋼桿的殘留應力。(10%)
- (鋼桿視為完全彈-塑性材料) (A-36 鋼降伏應力 $\sigma_Y = 250\text{ MPa}$)



參考解答:

$$1. \varepsilon_{\text{lat}} = \frac{37.5033 - 37.5}{37.5} = 0.0000880$$

$$\sigma = \frac{P}{A} = \frac{-40 \cdot 10^3}{50 \cdot 37.5 \cdot 10^{-6}} = -21.33 \cdot 10^6 \text{ (Pa)} = -21.33 \text{ (MPa)}$$

$$\sigma = E \cdot \varepsilon_{\text{long}} \Rightarrow \varepsilon_{\text{long}} = \frac{\sigma}{E} = \frac{-21.33 \cdot 10^6}{70 \cdot 10^9} = -0.00030476$$

$$\nu = -\frac{\varepsilon_{\text{lat}}}{\varepsilon_{\text{long}}} = -\frac{0.0000880}{-0.00030476} = 0.289$$

$$h' = h + \varepsilon_{\text{lat}} \cdot h = 50 + 50 \cdot 0.0000880 = 50.0044 \text{ (mm)}$$

$$2. (1) \text{ 中空棒截面積 } A = 50^2 - 40^2 = 900 \text{ (mm}^2\text{)}$$

$$\sigma = \frac{P}{A} = \frac{100 \cdot 10^3}{900 \cdot 10^{-6}} = 111.11 \cdot 10^6 \text{ (Pa)} = 111.11 \text{ (MPa)} \text{ (在彈性範圍內)}$$

由應力-應變圖可知

$$E = \frac{250}{0.00125} = 200 \cdot 10^3 \text{ (MPa)} = 200 \text{ (GPa)}$$

$$\delta = \frac{\sigma \cdot L}{E} = \frac{111.11 \cdot 10^{-3} \cdot 0.6}{200} = 0.33333 \cdot 10^{-3} \text{ (m)} = 0.33333 \text{ (mm)}$$

$$(2) \sigma = \frac{P}{A} = \frac{360 \cdot 10^3}{900 \cdot 10^{-6}} = 400 \cdot 10^6 \text{ (Pa)} = 400 \text{ (MPa)} \text{ (已降伏)}$$

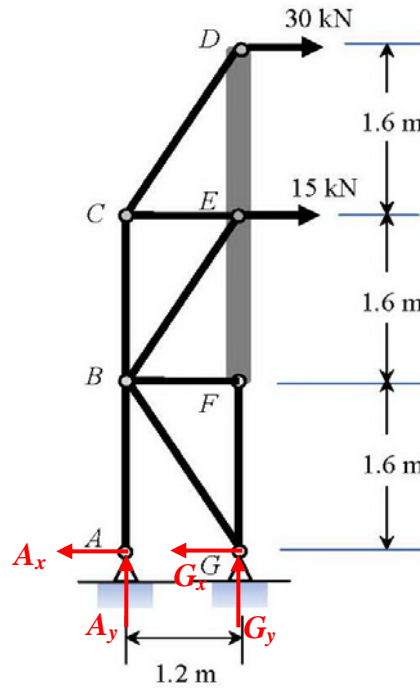
$$\frac{\varepsilon - 0.00125}{400 - 250} = \frac{0.05 - 0.00125}{500 - 250} \Rightarrow \varepsilon = 0.0305$$

$$\text{外力釋放後, 其沿彈性路徑的恢復量 } \varepsilon_r = \frac{400 \cdot 10^{-3}}{200} = 0.002$$

$$\text{永久應變 } \varepsilon_p = \varepsilon - \varepsilon_r = 0.0285$$

$$\text{永久伸長量 } \delta_p = \varepsilon_p \cdot L = 0.0285 \cdot 600 = 17.1 \text{ (mm)}$$

3.



(1) \because AB 桿件屬二力構件

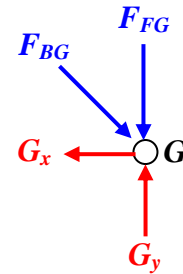
$$\therefore A_x = 0$$

$$\sum F_x = 0 \Rightarrow G_x = 45 \text{ (kN)}$$

$$\sum M_A = 0 \Rightarrow G_y \cdot 1.2 - 30 \cdot 4.8 - 15 \cdot 3.2 = 0$$

$$\Rightarrow G_y = 160 \text{ (kN)}$$

$$\sum F_y = 0 \Rightarrow A_y = -160 \text{ (kN)}$$



$$(2) \sum F_x = 0 \Rightarrow F_{BG} \cdot \frac{3}{5} - G_x = 0 \Rightarrow F_{BG} = \frac{5}{3} G_x = 75 \text{ (kN)}$$

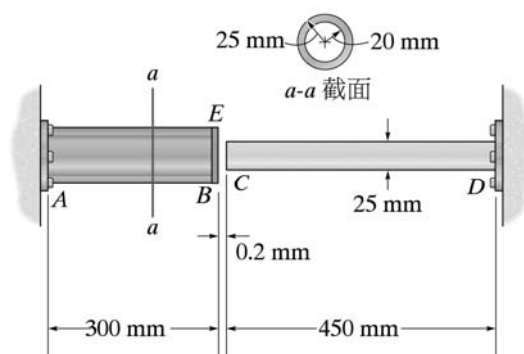
$$\sum F_y = 0 \Rightarrow F_{FG} + \frac{4}{5} F_{BG} - G_y = 0 \Rightarrow F_{FG} = G_y - \frac{4}{5} F_{BG} = 100 \text{ (kN)}$$

$$\sigma_{allow} = \frac{F_{BG}}{A} \Rightarrow A = \frac{F_{BG}}{\sigma_{allow}} = \frac{75 \cdot 10^3}{120} = 625 \text{ (mm}^2\text{)}$$

$$(3) G = \frac{E}{2(1+\nu)} \Rightarrow E = 2(1+\nu)G = 2 \cdot (1+0.3) \cdot 77.2 = 200.72 \text{ (GPa)}$$

$$\delta_{FG} = \frac{F_{FG} L_{FG}}{AE} = \frac{100 \cdot 10^3 \cdot 1600}{\pi \cdot 20^2 \cdot 10^{-6} \cdot 200.72 \cdot 10^9} = 0.6343 \text{ (mm)}$$

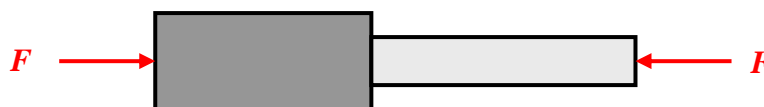
4. (1)



$$(\delta_T)_{AB} = \alpha_{ma} \cdot \Delta T \cdot L_{AB} = 26 \cdot 10^{-6} \cdot (80 - 30) \cdot 300 = 0.39 \text{ (mm)}$$

$$(\delta_T)_{CD} = \alpha_{al} \cdot \Delta T \cdot L_{CD} = 24 \cdot 10^{-6} \cdot (80 - 30) \cdot 450 = 0.54 \text{ (mm)}$$

\therefore 可知當溫度上升至 80°C 時， B 點會頂到 C 點



$$\delta = [(\delta_T)_{AB} - (\delta_F)_{AB}] + [(\delta_T)_{CD} - (\delta_F)_{CD}] = 0.2$$

$$\Rightarrow \left(0.39 - \frac{F \cdot 300}{\pi(25^2 - 20^2) \cdot 10^{-6} \cdot 44.7 \cdot 10^9}\right) + \left(0.54 - \frac{F \cdot 450}{\pi \cdot 12.5^2 \cdot 10^{-6} \cdot 68.9 \cdot 10^9}\right) = 0.2$$

$$\Rightarrow F = 32017.60 \text{ (N)} = 32.02 \text{ (kN)}$$

$$\sigma_{AB} = \frac{F}{A_{AB}} = \frac{32017.6}{\pi(25^2 - 20^2) \cdot 10^{-6}} = 45.30 \cdot 10^6 \text{ (Pa)} = 45.30 \text{ (MPa)}$$

$$\sigma_{CD} = \frac{F}{A_{CD}} = \frac{32017.6}{\pi \cdot 12.5^2 \cdot 10^{-6}} = 65.23 \cdot 10^6 \text{ (Pa)} = 65.23 \text{ (MPa)}$$

(2)

$$(\sigma_Y)_{ma} = \frac{F}{A_{AB}} = 152 \text{ MPa} \Rightarrow F = 152 \cdot 10^6 \cdot \pi(25^2 - 20^2) \cdot 10^{-6} = 107442.47 \text{ (N)}$$

$$(\sigma_Y)_{al} = \frac{F}{A_{CD}} = 255 \text{ MPa} \Rightarrow F = 255 \cdot 10^6 \cdot \pi \cdot 12.5^2 \cdot 10^{-6} = 125172.83 \text{ (N)}$$

$\therefore F$ 最大為 107442.47 (N)

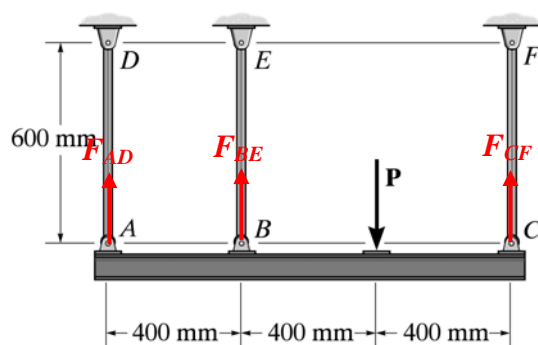
$$\text{又 } \delta = [(\delta_T)_{AB} - (\delta_F)_{AB}] + [(\delta_T)_{CD} - (\delta_F)_{CD}] = 0.2$$

$$\Rightarrow 26 \cdot 10^{-6} \cdot (T - 30) \cdot 300 - \frac{107442.47 \cdot 300}{\pi(25^2 - 20^2) \cdot 10^{-6} \cdot 44.7 \cdot 10^9}$$

$$+ 24 \cdot 10^{-6} \cdot (T - 30) \cdot 450 - \frac{107442.47 \cdot 450}{\pi \cdot 12.5^2 \cdot 10^{-6} \cdot 68.9 \cdot 10^9} = 0.2$$

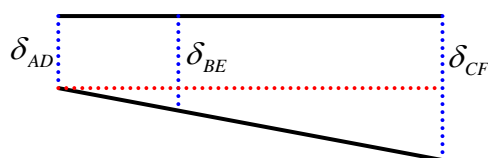
$$\Rightarrow T = 172 \text{ (}^\circ\text{C)}$$

5. (1)



$$\sum F_y = 0 \Rightarrow F_{AD} + F_{BE} + F_{CF} = P \quad \dots\dots (a)$$

$$\sum M_A = 0 \Rightarrow F_{BE} \cdot 400 + F_{CF} \cdot 1200 - P \cdot 800 = 0 \Rightarrow F_{BE} + 3F_{CF} = 2P \quad \dots\dots (b)$$



由幾何位移可看出相容方程為

$$\frac{\delta_{BE} - \delta_{AD}}{400} = \frac{\delta_{CF} - \delta_{AD}}{1200}$$

$$\Rightarrow 3\delta_{BE} - 2\delta_{AD} - \delta_{CF} = 0$$

$$\Rightarrow 3 \frac{F_{BE} \cdot L}{AE} - 2 \frac{F_{AD} \cdot L}{AE} - \frac{F_{CF} \cdot L}{AE} = 0$$

$$\Rightarrow 3F_{BE} - 2F_{AD} - F_{CF} = 0 \quad \dots\dots (c)$$

由解(a)、(b)、(c)聯立方程可得 $F_{BE} = \frac{2}{7}P$, $F_{CF} = \frac{4}{7}P$, $F_{AD} = \frac{1}{7}P$

$$\therefore F_{BE} = \frac{2}{7} \cdot 230 = 65.71 \text{ (kN)}$$

$$F_{CF} = \frac{4}{7} \cdot 230 = 131.43 \text{ (kN)}$$

$$F_{AD} = \frac{1}{7} \cdot 230 = 32.86 \text{ (kN)}$$

$$\sigma_{BE} = \frac{F_{BE}}{A} = \frac{65.71 \cdot 10^3}{\pi \cdot 12.5^2 \cdot 10^{-6}} = 133.87 \cdot 10^6 \text{ (Pa)} = 133.87 \text{ (MPa)} < \sigma_Y$$

$$\sigma_{CF} = \frac{F_{CF}}{A} = \frac{131.43 \cdot 10^3}{\pi \cdot 12.5^2 \cdot 10^{-6}} = 267.74 \cdot 10^6 \text{ (Pa)} = 267.74 \text{ (MPa)} > \sigma_Y$$

$$\sigma_{AD} = \frac{F_{AD}}{A} = \frac{32.86 \cdot 10^3}{\pi \cdot 12.5^2 \cdot 10^{-6}} = 66.94 \cdot 10^6 \text{ (Pa)} = 66.94 \text{ (MPa)} < \sigma_Y$$

$\therefore \sigma_{CF} > \sigma_Y$ 表示 CF 桿已降服，故須力量重分配

$$\therefore F'_{CF} = \sigma_Y \cdot A = 250 \cdot 10^6 \cdot \pi \cdot 12.5^2 \cdot 10^{-6} = 122718.46 \text{ (N)} = 122.72 \text{ (kN)}$$

$$\sum M_A = 0 \Rightarrow F'_{BE} + 3F'_{CF} = 2P \Rightarrow F'_{BE} = 2P - 3F'_{CF} = 91.84 \text{ (kN)}$$

$$\sum F_y = 0 \Rightarrow F'_{AD} + F'_{BE} + F'_{CF} = P \Rightarrow F'_{AD} = P - F'_{CF} - F'_{BE} = 15.44 \text{ (kN)}$$

$$\sigma'_{BE} = \frac{F'_{BE}}{A} = \frac{91.84 \cdot 10^3}{\pi \cdot 12.5^2 \cdot 10^{-6}} = 187.10 \cdot 10^6 \text{ (Pa)} = 187.10 \text{ (MPa)} < \sigma_Y$$

$$\sigma'_{AD} = \frac{F'_{AD}}{A} = \frac{15.44 \cdot 10^3}{\pi \cdot 12.5^2 \cdot 10^{-6}} = 31.45 \cdot 10^6 \text{ (Pa)} = 31.45 \text{ (MPa)} < \sigma_Y$$

$$(2) (\sigma_{CF})_r = \sigma'_{CF} - \sigma_{BE} = 250 - 267.74 = -17.74 \text{ (MPa)}$$

$$(\sigma_{BE})_r = \sigma'_{BE} - \sigma_{BE} = 187.10 - 133.87 = 53.23 \text{ (MPa)}$$

$$(\sigma_{AD})_r = \sigma'_{AD} - \sigma_{AD} = 31.45 - 66.94 = -35.49 \text{ (MPa)}$$